



PI Control of MIMO Stable Nonlinear Plants Using Projected Dynamical Systems Theory

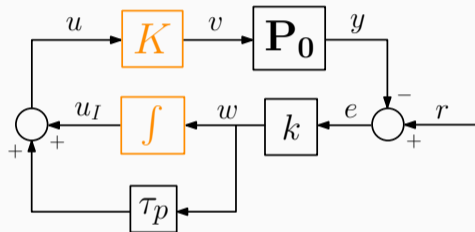
Pietro Lorenzetti (ESR 4)

ConFlex Consortium's 4th Network Meeting (August 4th-10th, 2021)

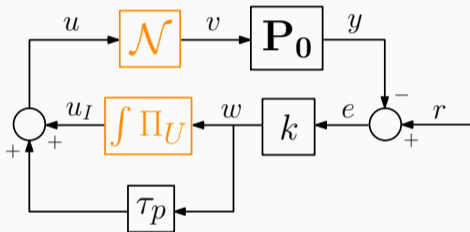
Supervisor George Weiss **Co-Supervisor** Enrique Zuazua

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Classical PI control loop



Saturating PI control loop



where $y, r, e, w, u_I, u \in \mathbb{R}^p$, $v \in \mathbb{R}^m$, $k, \tau_p > 0$, $K \in \mathbb{R}^{m \times p}$.

Keywords Anti-Windup, Singular Perturbations, Projected Dynamical Systems.

1. Projected Dynamical Systems

How is $\Pi_U(u_I, w)$ defined?

3. Stability Analysis

How to derive stability results?

2. Problem Formulation

What is the control problem that we address?

4. Numerical Example

Power Regulation for a Grid-Connected Synchronverter

Projected Dynamical Systems

Definition 1.* For a closed convex set $U \subset \mathbb{R}^p$, let the projection operator $P_U(w)$ be defined for all $w \in \mathbb{R}^p$ as

$$P_U(w) = \arg \min_{u \in U} \|w - u\|,$$

then we define $\Pi_U(u, w)$ for all $w \in \mathbb{R}^p$ and $u \in U$ as

$$\Pi_U(u, w) = \lim_{\delta \rightarrow 0} \frac{(P_U(u + \delta w) - u)}{\delta}.$$

*P. Dupuis. Large deviations analysis of reflected diffusions and constrained stochastic approximation algorithms in convex sets. *Stochastics*, 21(1):63-96, 1987.

Lemma 1.* Let the operator $\Pi_U(u, w)$ and the set U be as defined before. Then

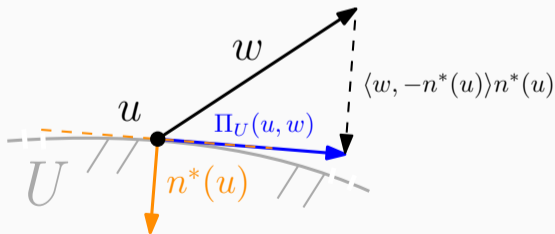
1. If $u \in U^\circ$, then $\Pi_U(u, w) = w$.
2. if $u \in \partial U$, then $\Pi_U(u, w) = w + \beta(u)n^*(u)$, where

$$n^*(u) = \arg \max_{n \in n(u)} \langle w, -n \rangle, \quad \text{and} \quad \beta(u) = \max\{0, \langle w, -n^*(u) \rangle\},$$

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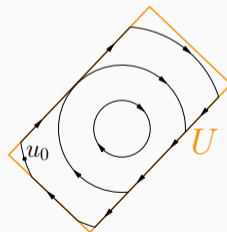
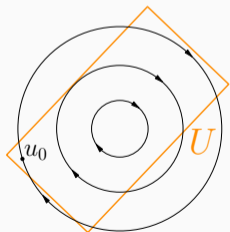
Definition 2.* Let $U \subset \mathbb{R}^p$ be a closed and convex set, and $F : U \rightarrow \mathbb{R}^p$ a vector field. Define a **projected dynamical system** $\text{PDS}(F, U)$ as the map $\Phi : U \times \mathbb{R} \mapsto U$, such that $\phi_{u_0}(t) = \Phi(u_0, t)$ is a Carathéodory solution of

$$\dot{\phi}_{u_0}(t) = \Pi_U(\phi_{u_0}(t), -F(\phi_{u_0}(t))), \quad \phi_{u_0}(0) = u_0. \quad (1)$$

*A. Nagurny and D. Zhang. *Projected Dynamical Systems and Variational Inequalities with Applications*. International Series in Operations Research & Management Science. Springer US, 1996.

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Theorem 1.* Let $U \subset \mathbb{R}^p$ be a closed and convex set. Assume that there exists a finite $B > 0$ such that the vector field $-F : U \rightarrow \mathbb{R}^p$ satisfies:

$$\begin{aligned}\|F(u)\| &\leq B(1 + \|u\|) \quad \forall u \in U, \\ \langle -F(u_1) + F(u_2), u_1 - u_2 \rangle &\leq B\|u_1 - u_2\|^2 \quad \forall u_1, u_2 \in U.\end{aligned}$$

Then:

1. For any $u_0 \in U$, there **exists a unique solution** $u : [0, \infty) \rightarrow U$ to the initial value problem (1).
2. If $u_n \rightarrow u_0$ as $n \rightarrow \infty$, then $u(t; u_n)$ converges to $u(t; u_0)$ uniformly on every compact set in $[0, \infty)$.

Control Problem Formulation

The nonlinear plant \mathbf{P}_0 to be controlled is described by:

$$\dot{x} = f_0(x, v), \quad y = g(x),$$

with $f_0 \in C^2(\mathbb{R}^n \times \mathcal{V}; \mathbb{R}^n)$, $g \in C^1(\mathbb{R}^n; \mathbb{R}^p)$, and $\mathcal{V} \subset \mathbb{R}^m$ ($m \geq p$) open domain.

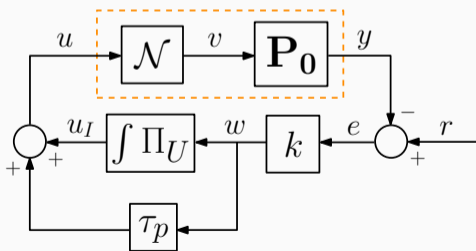
Control Objective

The control objective is to make the output signal y track a constant reference signal $r \in Y \subset \mathbb{R}^p$, while making sure that the input signal v converges to a steady-state value in a desired compact set $V \subset \mathbb{R}^m$ (e.g., determined by operational constraints).

The **closed-loop system** is described by

$$\dot{x} = f_0(x, \mathcal{N}(u_I + \tau_p k(r - g(x))))), \quad \dot{u}_I = \Pi_U(u_I, k(r - g(x))), \quad (2)$$

where $\mathcal{U} \subset \mathbb{R}^p$ is an open domain, $U \subset \mathcal{U}$ is compact and convex, $\mathcal{N} \in C^2(\mathcal{U}, \mathcal{V})$, $V = \mathcal{N}(U)$, $k > 0$ and $\tau_p \geq 0$, with state space $\mathbb{R}^n \times \mathcal{U}$.



Notation. Denote by

$$\mathcal{D}_r := \left\{ \begin{bmatrix} x \\ u_I \end{bmatrix} \in \mathbb{R}^n \times \mathcal{U} \mid u_I + \tau_p k(r - g(x)) \in \mathcal{U} \right\} .$$

Proposition 1. Consider the closed-loop system (2), with $k, \tau_p \in \mathbb{R}$, $r \in \mathbb{R}^p$. Then for every $\begin{bmatrix} x_0 \\ u_0 \end{bmatrix} \in \mathcal{D}_r$ with $u_0 \in U$, there exists $\tau \in (0, \infty]$ such that (2), with initial conditions $z(0) = \begin{bmatrix} x_0 \\ u_0 \end{bmatrix}$, has a **unique Carathéodory solution** (or state trajectory) z defined on $[0, \tau)$. If τ is finite and maximal (i.e., the state trajectory cannot be continued beyond τ), then $\limsup_{t \rightarrow \tau} \|z(t)\| = \infty$, or

$$\lim_{t \rightarrow \tau} (u_I(t) + \tau_p k(r - g(x(t)))) \in \partial \mathcal{U} .$$

Closed-Loop Stability Analysis

Assumption 1. There exists a function $\Xi \in C^1(\mathcal{V}; \mathbb{R}^n)$ such that

$$f_0(\Xi(v), v) = 0 \quad \forall v \in \mathcal{V}.$$

Moreover, the set of equilibrium points $\{\Xi(v) \mid v \in \mathcal{V}\}$ is **uniformly exponentially stable**. This means that there exist $\varepsilon_0 > 0$, $\lambda > 0$ and $\rho \geq 1$ such that for each constant input $v_0 \in \mathcal{V}$, the following holds:

If $\|x(0) - \Xi(v_0)\| \leq \varepsilon_0$, then for every $t \geq 0$,

$$\|x(t) - \Xi(v_0)\| \leq \rho e^{-\lambda t} \|x(0) - \Xi(v_0)\|.$$

Notation. Let $G(v) := g(\Xi(v)) \in C^1(\mathcal{V}; \mathbb{R}^p)$ denote the steady-state input-output map corresponding to \mathbf{P}_0 .

Assumption 2. The plant \mathbf{P}_0 satisfies Assumption 1. Moreover, there exist an open set $\mathcal{U} \subset \mathbb{R}^p$, a function $\mathcal{N} \in C^2(\mathcal{U}, \mathcal{V})$, and $\mu > 0$ such that

$$\langle G(\mathcal{N}(u_1)) - G(\mathcal{N}(u_2)), u_1 - u_2 \rangle \geq \mu \|u_1 - u_2\|^2$$

for all $u_1, u_2 \in \mathcal{U}$, i.e., $G \circ \mathcal{N}$ is **strictly monotone**.

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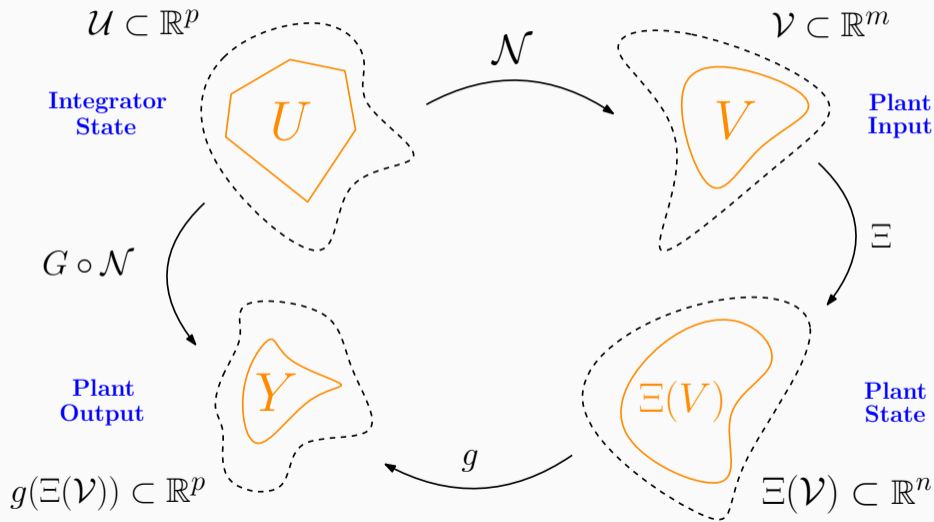
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for all $u_1, u_2 \in \mathcal{U}$, i.e., $G \circ \mathcal{N}$ is **strictly monotone**.

We denote $Y = G(\mathcal{N}(U))$, and, for any $r \in Y$, we define

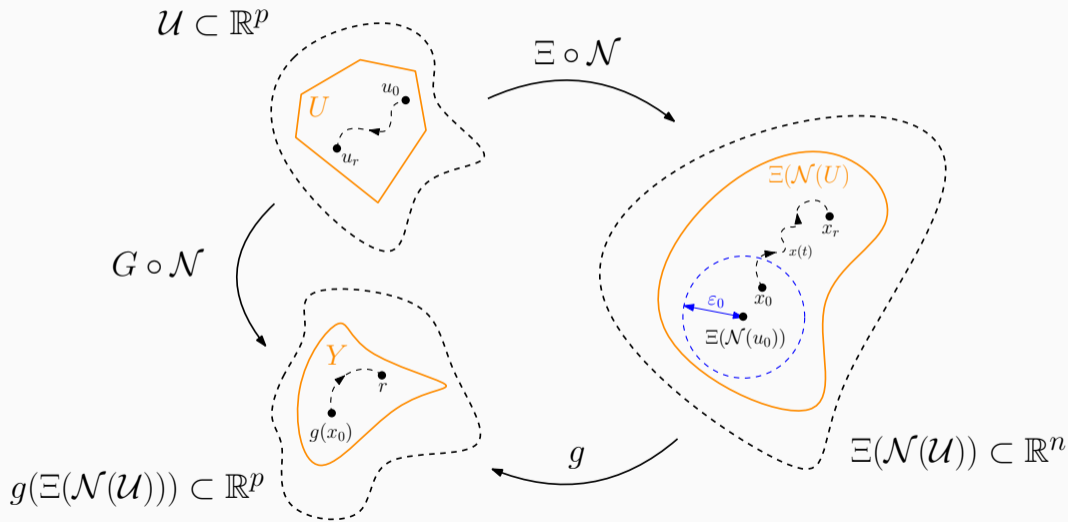
$$u_r := (G \circ \mathcal{N})^{-1}(r) \quad x_r := \Xi(\mathcal{N}(u_r)).$$



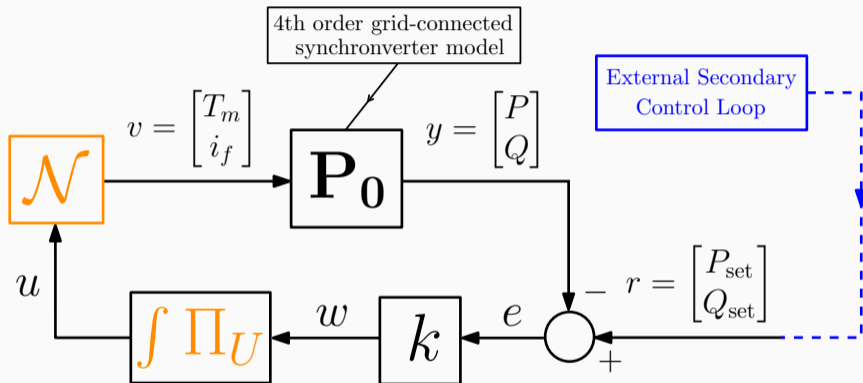
Theorem 2. Consider the closed-loop system (2), where \mathbf{P}_0 satisfies Assumption 2. Then there exists a $\kappa > 0$ such that if the gain $k \in (0, \kappa]$, then for any $r \in Y = G(\mathcal{N}(U))$, $(\Xi(\mathcal{N}(u_r)), u_r)$ is a (locally) exponentially stable equilibrium point of the closed-loop system (2), with state space $X = \mathbb{R}^n \times \mathcal{U}$. If the initial state $\begin{bmatrix} x_0 \\ u_0 \end{bmatrix} \in \mathcal{D}_r$, of the closed-loop system satisfies $u_0 \in U$ and $\|x_0 - \Xi(\mathcal{N}(u_0))\| \leq \varepsilon_0$, then

$$x(t) \rightarrow \Xi(\mathcal{N}(u_r)), \quad u_I(t) \rightarrow u_r, \quad y(t) \rightarrow r,$$

and this convergence is at an **exponential rate**.



Numerical Example



where $m = p = 2$, and $n = 4$.

The plant \mathbf{P}_0 , with state $x = [i_d \ i_q \ \omega \ \delta]^\top \in \mathbb{R}^4$, is described by the equations*

$$H\dot{x} = A(x, v)x + h(x, v), \quad y = g(x),$$

with

$$H = \begin{bmatrix} L & 0 & 0 & 0 \\ 0 & L & 0 & 0 \\ 0 & 0 & J & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \quad h(x, v) = \begin{bmatrix} V \sin \delta \\ V \cos \delta \\ T_m + D_p \omega_n \\ -\omega_g \end{bmatrix},$$

$$A(x, v) = \begin{bmatrix} -R & \omega L & 0 & 0 \\ -\omega L & -R & -mi_f & 0 \\ 0 & mi_f & -D_p & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}, \quad g(x) = -V \begin{bmatrix} \cos \delta & \sin \delta \\ -\sin \delta & \cos \delta \end{bmatrix} \begin{bmatrix} i_q \\ i_d \end{bmatrix}.$$

*P. Lorenzetti, Z. Kustanovich, S. Shivratri, and G. Weiss. "The equilibrium points and stability of grid-connected synchronverters," *IEEE Trans. Power Systems*, to appear in 2021.

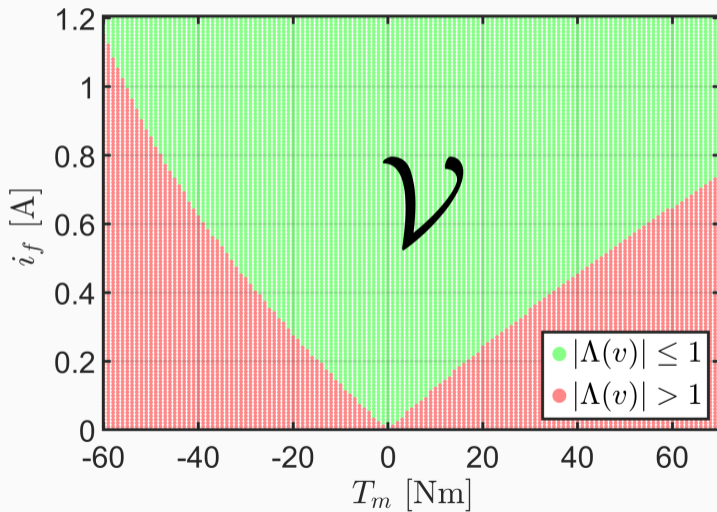
Parameter	Numerical Value
ω_g	100π rad/sec (50 Hz)
V	$230\sqrt{3}$ Volts
J	0.2 Kg·m ² /rad
D_p	3 N·m/(rad/sec)
R	1.875 Ω
L	56.75 mH
m	3.5 H
ω_n	100π rad/sec (50 Hz)

The function $\Xi : \mathcal{V} \rightarrow \mathbb{R}^4$ is given by

$$\Xi(v) = \begin{bmatrix} -\frac{T_m \omega_g}{mi_f p} + \frac{V \sin(\arccos \Lambda(v) - \phi)}{R} \\ -\frac{T_m}{mi_f} \\ \omega_g \\ \arccos \Lambda(v) - \phi \end{bmatrix}, \quad \text{where}$$

$$\phi \in \left(0, \frac{\pi}{2}\right) \quad \text{s. t.} \quad \tan \phi = \frac{\omega_g L}{R}, \quad \Lambda(v) = -\frac{T_m}{mi_f} \frac{L \sqrt{p^2 + \omega_g^2}}{V} + \frac{mi_f \omega_g p}{V \sqrt{p^2 + \omega_g^2}},$$

$$p = \frac{R}{L}, \quad \text{and} \quad \mathcal{V} = \{(T_m, i_f) \in \mathbb{R} \times (0, \infty) \mid |\Lambda(v)| \leq 1\}.$$



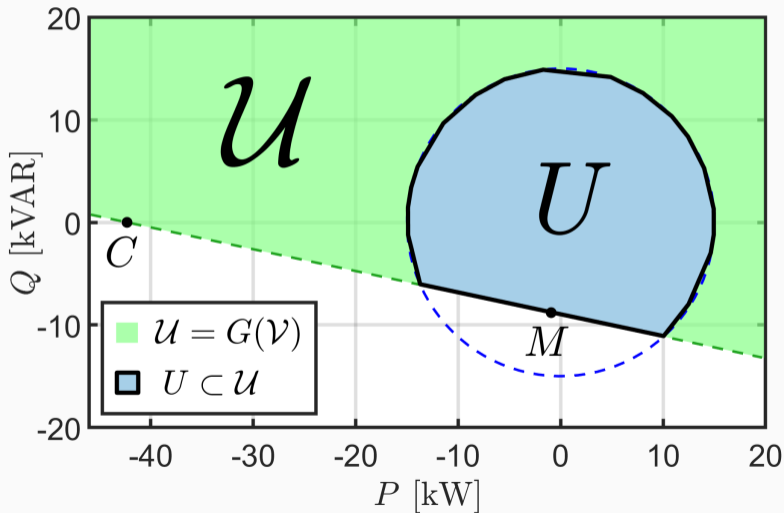
We choose $\mathcal{N} = G_{\text{right}}^{-1} \in C^2(G(\mathcal{V}), \mathcal{V})$, described by the equation

$$\mathcal{N}(u) = \begin{bmatrix} \frac{4R^2\|u-C\|^2 - V^4}{4V^2\omega_g R} \\ \frac{\|u-M\|\|Z\|}{V\omega_g m} \end{bmatrix},$$

where

$$C = \begin{bmatrix} -\frac{V^2}{2R} \\ 0 \end{bmatrix}, \quad Z = \begin{bmatrix} R \\ \omega_g L \end{bmatrix}, \quad M = -\frac{V^2}{\|Z\|^2} Z,$$

so that Assumption 2 is satisfied ($G \circ \mathcal{N} = I$) with $\mathcal{U} = G(\mathcal{V})$.



An alternative choice to $\mathcal{N} = G_{\text{right}}^{-1}$ could be, e.g., $\mathcal{N} = K \in \mathbb{R}^{2 \times 2}$ given by

$$K = \begin{bmatrix} \frac{1}{50} & 0 \\ 0 & \frac{1}{5000} \end{bmatrix}. \quad (3)$$

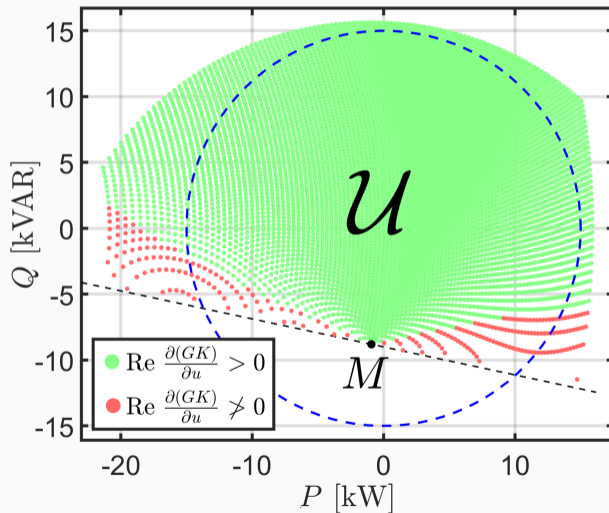
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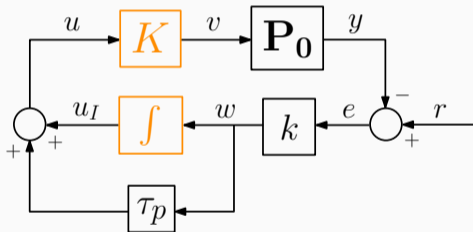
The (strict) monotonicity of $G \circ \mathcal{N} \in C^1(\mathcal{U}, \mathbb{R}^p)$ is equivalent to the fact that $\text{Re} \frac{\partial(G \circ \mathcal{N})}{\partial u}$ is strongly positive, i.e., there exists a $\mu > 0$ such that

$$\left\langle \frac{\partial(G \circ \mathcal{N})}{\partial u} w, w \right\rangle \geq \mu \|w\|^2 \quad \forall w \in \mathbb{R}^p, \forall u \in \mathcal{U}.$$

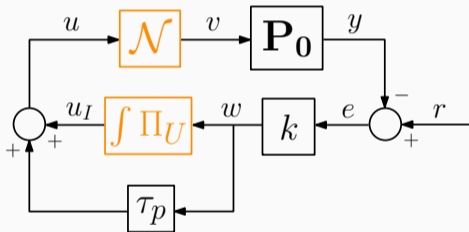
Assumption 2 - The sets \mathcal{U} and \mathcal{U} (Alternative Choice)



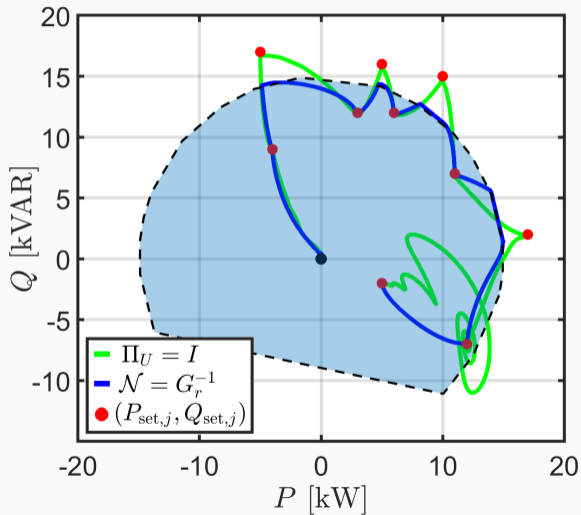
Classical PI control loop

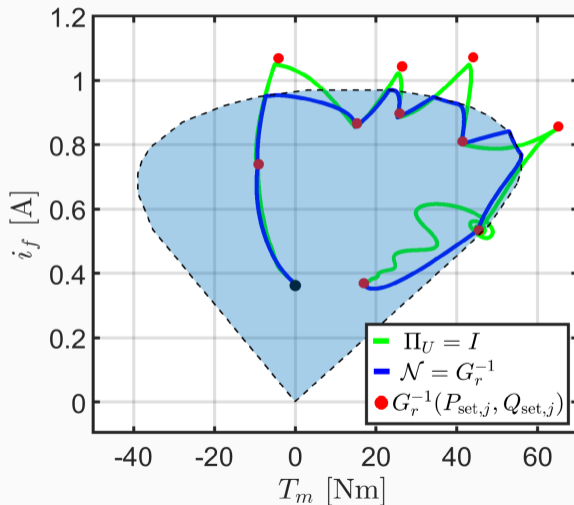


Saturating PI control loop



where $\tau_p = 0$, $k = 1$ (on the left), $k = 2$ (on the right).





MIMO Sat. Integrator

Anti-Windup

Proj. Dyn. Systems

Stability Analysis

Singular Perturbation




Novel $\mathcal{N} = G_{\text{right}}^{-1}$



Application

Power Regulation of a

G.-C. Synchronverter

Publications & Awards

-  P. Lorenzetti, Z. Kustanovich, S. Shivratri, and G. Weiss.
“The equilibrium points and stability of grid-connected synchronverters,”
IEEE Trans. Power Systems, to appear in 2021 (available on *arXiv*).
-  P. Lorenzetti and G. Weiss.
“Saturating PI control of stable nonlinear systems using singular perturbations,”
under review with *IEEE Trans. Aut. Control*, 2020 (available on *arXiv*).
-  P. Lorenzetti and G. Weiss.
“PI Control of stable nonlinear plants using projected dynamical systems theory,”
about to be submitted.

-  P. Lorenzetti and G. Weiss.
“Integral control of stable MIMO nonlinear systems with input constraints,”
to appear in the *Proc. of the 3rd MICNON Conference, Tokyo, September, 2021.*
-  P. Lorenzetti, G. Weiss and V. Natarajan.
“Integral control of stable nonlinear systems based on singular perturbations”,
IFAC-PapersOnLine, vol. 53, pp. 6157-6164, 2020.




GSC 2021 (Graduate Students in System & Control 2021) Award for the talk *“The Saturating Integrator”*, conferred by the Israeli Association for Automatic Control (IAAC) at the Technion (Haifa), in May 2021



Finalist for the Young Author Prize at the MICNON Conference 2021 with the contribution *“Integral control of stable MIMO nonlinear systems with input constraints”* (final winner to be chosen in September 2021).

Finalist for the Young Author Prize at the IFAC World Congress 2020 with the contribution *“Integral control of stable nonlinear systems based on singular perturbations”*.

Future?

Thanks for your attention!

-  P. Dupuis.
“Large deviations analysis of reflected diffusions and constrained stochastic approximation algorithms in convex sets,”
Stochastics, vol. 21, pp. 63-96, 1987.
-  P. Lorenzetti, Z. Kustanovich, S. Shivratri, and G. Weiss.
“The equilibrium points and stability of grid-connected synchronverters,”
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-  P. Lorenzetti and G. Weiss.
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-  A. Nagurney and D. Zhang.
Projected Dynamical Systems and Variational Inequalities with Applications,
Springer Science & Business Media, 1995.
-  V. Natarajan and G. Weiss.
“Almost global asymptotic stability of a grid-connected synchronous generator,”
Math. of Control, Signals and Systems, vol. 30, 2018.

Numerical Results - The Quantities P and Q in Time

