

Low order approximation of flexible structures

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Motion system description

■ Motivation

Motion system description

- Motivation
- System description in frequency domain

$$G(s) = \frac{G_2}{s^2} + \frac{G_1}{s} + \underbrace{G_0 + G_{st}(s)}_{G_{flex}(s)}, \quad s \in \mathbb{C}. \quad (1)$$

Definition

For the system described by the transfer function (1), we define **the compliance function** by the following limit:

$$G_0 = \lim_{s \rightarrow 0} \left(G(s) - \frac{G_2}{s^2} - \frac{G_1}{s} \right). \quad (2)$$

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$$\omega_{assumed}(t) = \omega_2 \frac{t^2}{2} + \omega_1 t + \omega_0 + \omega_{st}(t). \quad (3)$$

Cauchy problem

Let X and U be an infinite dimensional Hilbert space. The general damped model to be considered is described as:

$$\begin{aligned}\ddot{\omega}(t) + d\mathcal{A}_0\dot{\omega}(t) + \mathcal{A}_0\omega(t) &= Bu(t), \\ \omega(0) = 0, \quad \dot{\omega}(0) &= 0,\end{aligned}\tag{4}$$

where $\mathcal{A}_0 : \mathbf{D}(\mathcal{A}_0) \subseteq X \rightarrow X$ be a self-adjoint, non-negative operator with a compact resolvent. $B : U \rightarrow X$.

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$$\dot{z}(t) = \underbrace{\begin{bmatrix} 0 & I \\ -\mathcal{A}_0 & -d\mathcal{A}_0 \end{bmatrix}}_{A_0} z(t) + \begin{bmatrix} 0 \\ B \end{bmatrix} u(t),$$

where $z = [\overset{\omega}{\omega}] \in Z := \mathbf{D}(\mathcal{A}_0^{\frac{1}{2}}) \times X$ and $\mathbf{D}(A_0) = \mathbf{D}(\mathcal{A}_0) \times \mathbf{D}(\mathcal{A}_0^{\frac{1}{2}})$.

Time domain approach

$$\mathcal{X} = \overline{\text{span}}\{\varphi_1, \varphi_2, \varphi_3, \dots, \varphi_{n+1}, \dots\}.$$

By taking $u(t) = u_0, t \geq 0$ and the assumed output, the following set of equations are obtained:

$$\mathcal{A}_0 \omega_2 = 0,$$

$$\mathcal{A}_0 \omega_1 + d \mathcal{A}_0 \omega_2 = 0,$$

$$\mathcal{A}_0 \omega_0 + d \mathcal{A}_0 \omega_1 + \omega_2 = B u_0,$$

$$\ddot{\omega}_{st}(t) + d \mathcal{A}_0 \dot{\omega}_{st}(t) + \mathcal{A}_0 \omega_{st}(t) = 0,$$

$$\omega_{st}(0) = -\omega_0, \quad \dot{\omega}_{st}(0) = -\omega_1.$$

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$$\mathcal{A}_0 \varphi_k = \lambda_k \varphi_k, \quad \text{with } \begin{cases} \lambda_k > 0, & \text{if } k \geq N + 1 \\ \lambda_k = 0, & 1 \leq k \leq N \end{cases},$$

where λ_k are the eigenvalues of \mathcal{A}_0 .

Time domain approach

Theorem

$$\omega_2 = \sum_{k=1}^N \alpha_k \varphi_k \quad \omega_1 = \mathbf{0}, \quad \omega_0 = \sum_{k=N+1}^{\infty} \beta_k \varphi_k,$$

where

$$\alpha_k = \langle \varphi_k, \mathbf{B}u_0 \rangle, \quad \beta_k = \frac{\langle \varphi_k, \mathbf{B}u_0 \rangle}{\lambda_k}.$$

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■ Frequency domain approach

The transfer function from u to ω of (4) equals

$$G(s) = (s^2 + sd\mathcal{A}_0 + \mathcal{A}_0)^{-1}B.$$

since $\omega(s) = G(s)u_0$ and using the orthonormal basis of X ,

$$\omega(s) = \sum_{k=1}^{\infty} \langle \varphi_k, \omega(s) \rangle \varphi_k = \sum_{k=1}^{\infty} \frac{\langle \varphi_k, \mathbf{B}u_0 \rangle}{s^2 + sd\lambda_k + \lambda_k} \varphi_k.$$

Frequency domain approach

By separating the calculation for $\lambda_k = 0$ and $\lambda_k > 0$, we have:

$$\begin{aligned}\omega(s) &= \sum_{k=0}^N \langle \varphi_k, \omega \rangle \varphi_k + \sum_{k=N+1}^{\infty} \langle \varphi_k, \omega \rangle \varphi_k \\ &= \sum_{k=0}^N \frac{\langle \varphi_k, BU_0 \rangle}{s^2} \varphi_k + \sum_{k=N+1}^{\infty} \left[\frac{a_k}{s - \mu_{k,1}} + \frac{b_k}{s - \mu_{k,2}} \right] \varphi_k.\end{aligned}$$

Hence

$$G_2 U_0 = \sum_{k=0}^N \langle \varphi_k, BU_0 \rangle \varphi_k, \quad G_1 = 0,$$

$$G_0 U_0 = \sum_{k=N+1}^{\infty} \frac{\langle \varphi_k, BU_0 \rangle}{\mu_{k,1} \mu_{k,2}} \varphi_k = \sum_{k=N+1}^{\infty} \frac{\langle \varphi_k, BU_0 \rangle}{\lambda_k} \varphi_k.$$

Boundary control problem

Let's consider:

$$\begin{aligned}\ddot{\omega}(t) + d\mathcal{A}\dot{\omega}(t) + \mathcal{A}\omega(t) &= 0, & \omega(0) = 0, \dot{\omega}(0) = 0, & \quad (5) \\ \mathcal{B}_0\omega(t) &= 0, \\ \mathcal{B}_c\omega(t) &= u(t).\end{aligned}$$

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$$\mathcal{A}_0 = \mathcal{A}, \quad \mathbf{D}(\mathcal{A}_0) = \{z \in \mathbf{D}(\mathcal{A}) \mid \mathcal{B}_0z = 0 \text{ and } \mathcal{B}_cz = 0\}.$$

Let's define $B \in \mathcal{L}(U, X)$ such that for all $u \in U$, $Bu \in \mathbf{D}(\mathcal{A})$, the operator $\mathcal{A}B$ is an element of $\mathcal{L}(U, X)$ and,

$$\mathcal{B}_0Bu = 0, \text{ and } \mathcal{B}_cBu = u.$$

$$\langle z, \mathcal{A}x \rangle_X = \langle \mathcal{A}_0z, x \rangle_X - \langle Qz, \mathcal{B}_cx \rangle_U, \quad x \in \mathbf{D}(\mathcal{A}) \cap \ker \mathcal{B}_0, z \in \mathbf{D}(\mathcal{A}_0),$$

where Q is a linear operator from $\mathbf{D}(\mathcal{A})$ to U .

$$\begin{aligned}\ddot{v}(t) + d\mathcal{A}_0\dot{v}(t) + \mathcal{A}_0v(t) &= -B\ddot{u}(t) - d\mathcal{A}B\dot{u}(t) - \mathcal{A}Bu(t), & (6) \\ v(0) = \epsilon - Bu_0, \dot{v}(0) &= -B\dot{u}_0.\end{aligned}$$

Time domain approach

$$\mathcal{A}\omega_2 = 0,$$

$$\mathcal{A}\omega_1 + d\mathcal{A}\omega_2 = 0,$$

$$\mathcal{A}\omega_0 + d\mathcal{A}\omega_1 + \omega_2 = 0,$$

$$\ddot{\omega}_{st}(t) + d\mathcal{A}\dot{\omega}_{st}(t) + \mathcal{A}\omega_{st}(t) = 0,$$

$$\omega_{st}(0) = \epsilon - \omega_0, \quad \dot{\omega}_{st}(0) = -\omega_1.$$

$$\begin{cases} \mathcal{B}_0\omega_2 = 0, & \mathcal{B}_0\omega_1 = 0, & \mathcal{B}_0\omega_0 = 0, & \mathcal{B}_0\omega_{st} = 0, \\ \mathcal{B}_c\omega_2 = 0, & \mathcal{B}_c\omega_1 = 0, & \mathcal{B}_c\omega_0 = u_0, & \mathcal{B}_c\omega_{st} = 0. \end{cases}$$

Theorem

$$\omega_2 = \sum_{k=1}^N \alpha_k \varphi_k \quad \omega_1 = 0, \quad \omega_0 = \sum_{k=N+1}^{\infty} \beta_k \varphi_k,$$

$$\alpha_k = \langle u_0, Q\varphi_k \rangle_U, \quad \beta_k = \frac{\langle Q\varphi_k, u_0 \rangle_U}{\lambda_k}.$$

Frequency domain approach

The transfer function from u to ω equals

$$G(s) = -(s^2 + sd\mathcal{A}_0 + \mathcal{A}_0)^{-1}(s^2B + d\mathcal{A}Bs + \mathcal{A}B) + B.$$

$$\omega(s) = \sum_{k=0}^N \left[\frac{1}{s} d \langle Q\varphi_k, u_0 \rangle + \frac{1}{s^2} \langle Q\varphi_k, u_0 \rangle \right] \varphi_k +$$

$$\sum_{k=N+1}^{\infty} \left[\langle Q\varphi_k, u_0 \rangle \left(\frac{d\mu_{k,1} + 1}{\mu_{k,2} - \mu_{k,1}} \frac{1}{s - \mu_{k,1}} + \frac{d\mu_{k,2} + 1}{\mu_{k,2} - \mu_{k,1}} \frac{1}{s - \mu_{k,2}} \right) \right] \varphi_k.$$

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Hence

$$G_2 u_0 = \sum_{k=1}^N \langle Q\varphi_k, u_0 \rangle \varphi_k, \quad G_1 u_0 = dG_2 u_0,$$

$$G_0 u_0 = \sum_{k=N+1}^{\infty} \frac{\langle Q\varphi_k, u_0 \rangle}{\lambda_k} \varphi_k.$$

One-dimensional Wave equation

$$\frac{\partial^2 \omega}{\partial t^2} = \frac{\partial^2 \omega}{\partial x^2} + d \frac{\partial^3 \omega}{\partial t \partial x^2},$$

$$\frac{\partial \omega}{\partial x}(0, t) = 0, \quad \frac{\partial \omega}{\partial x}(1, t) = u_0.$$

$$\omega(x, 0^+) = 0, \quad \frac{\partial \omega}{\partial t}(x, 0^+) = 0,$$

- Time domain approach

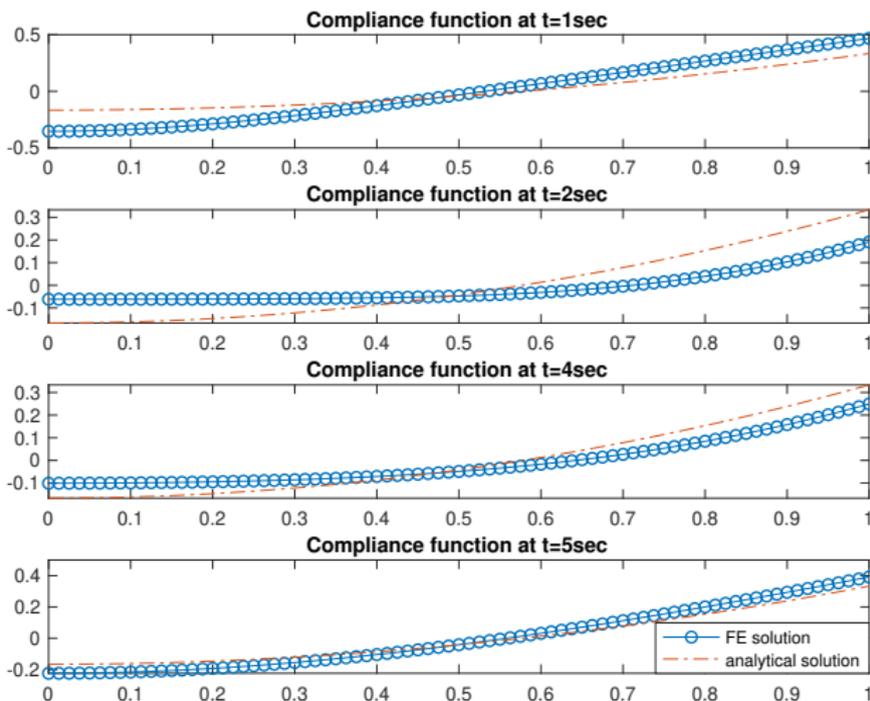
$$\begin{cases} \omega_1 = 0 \\ A_0 \omega_2 = 0, & \rightarrow \omega_2(x) = -u_0, \quad \omega_0(x) = -u_0 \frac{x^2}{2} + C_4. \\ A \omega_0 + \omega_2 = 0, \end{cases}$$

- Extra condition $\omega_{st}(x, 0^+) = -\omega_0(x)$

So ω_0 lies in the stable part of system

$$\int_0^1 \omega_{st}(t=0) dx = \int_0^1 -\omega_0(x) dx = 0, \rightarrow \omega_0(x) = \frac{1}{6} u_0 (-1 + 3x^2).$$

Wave equation-Time domain approach



Wave equation-Frequency domain approach

$$\begin{aligned}
 s^2 W(s, x) &= (ds + 1) \frac{d^2 W(s, x)}{dx^2}, \\
 \frac{dW(s, 0)}{dx} &= 0, \quad \frac{dW(s, 1)}{dx} = u_1.
 \end{aligned} \tag{7}$$

$$G(s) = \frac{\sqrt{1 + ds} \cosh\left(\frac{sx}{\sqrt{1+ds}}\right)}{s \sinh\left(\frac{s}{\sqrt{1+ds}}\right)},$$

For all $s \in \Omega = \left\{ s \in \mathbb{C} \mid s \neq \frac{-dk^2\pi^2 \pm k\pi\sqrt{d^2k^2\pi^2 - 4}}{2}, i = 1, 2, k = 0, 1, 2, \dots \right\}$.

Wave equation-Frequency domain approach

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$$G_2(x) = \lim_{s \rightarrow 0} (s^2 G(s)) = 1,$$

$$G_1(x) = \lim_{s \rightarrow 0} s(G(s) - \frac{G_2}{s^2}) = d,$$

$$G_0(x) = \lim_{s \rightarrow 0} (G(s) - \frac{G_2}{s^2} - \frac{d}{s}) = \frac{1}{6}(-1 + 3x^2).$$

Kirchhoff plate model

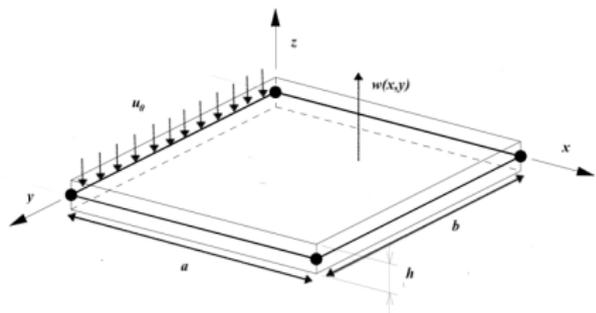
$$\rho h \ddot{w} + \underbrace{\kappa^T [D] \kappa}_{\mathcal{A}} \omega + \underbrace{c_d \kappa^T [D] \kappa}_{\mathcal{A}} \dot{\omega} = 0, \quad (x, y) \in \Omega \times [0, \infty)$$

■ where

$$\mathcal{K} = \begin{bmatrix} \frac{\partial^2}{\partial x^2} & \frac{\partial^2}{\partial y^2} & \frac{\partial^2}{\partial x \partial y} \end{bmatrix}^T,$$

■

$$[D] = \frac{Eh^3}{12(1-\nu^2)} \begin{bmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & \frac{1}{2}(1-\nu) \end{bmatrix}$$



Kirchhoff plate model-Time domain approach

$$\kappa^T [D] \kappa \omega_2 = 0,$$

$$\kappa^T [D] \kappa \omega_1 + d \kappa^T [D] \kappa \omega_2 = 0,$$

$$\kappa^T [D] \kappa \omega_0 + \omega_2 = 0,$$

$$\ddot{\omega}_{st}(t) + c_d \kappa^T [D] \kappa \dot{\omega}_{st}(t) + \kappa^T [D] \kappa \omega_{st}(t) = 0,$$

$$\omega_{st}(0) = \epsilon - \omega_0, \quad \dot{\omega}_{st}(0) = 0.$$

■ Boundary control problem

$$\mathcal{A}_0 = \kappa^T [D] \kappa \quad \text{with } \mathbf{D}(\mathcal{A}_0) = \mathbf{D}(\mathcal{A}) \cap \ker \mathcal{B}.$$

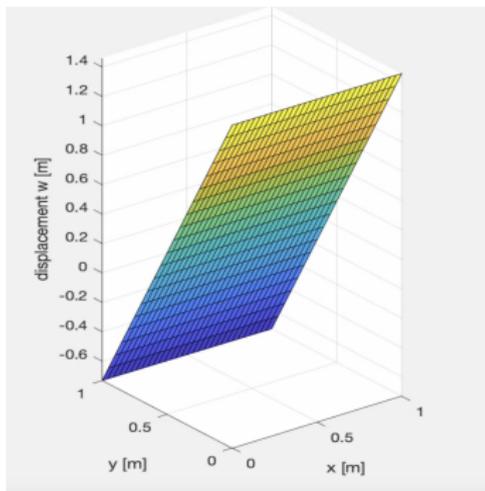
- Bu is defined by $Bu = b(x, y)u_0$ where $b(x, y)$ is a function and is contained in the domain of \mathcal{A} with $\mathcal{B}Bu_0 = u_0 \quad \forall u_0 \in \mathbb{R}$ and $\mathcal{A}B = I$.

$$\mathcal{A}_0 \omega_0 + \omega_2 = u_0 \mathbb{1}_\Omega(x, y).$$

$$\Delta^2 B(x, y) = 1.$$

Kirchhoff plate model-numerical solution

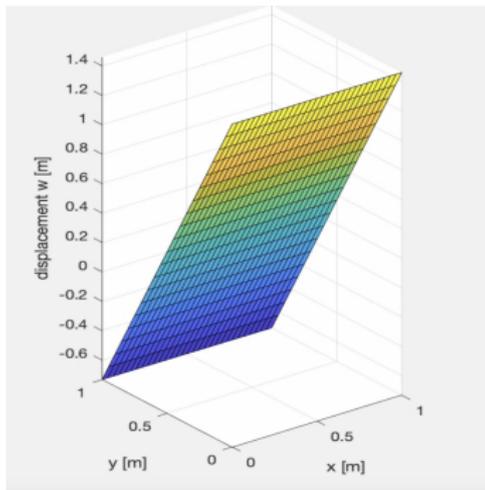
Inertia function ω_2^1



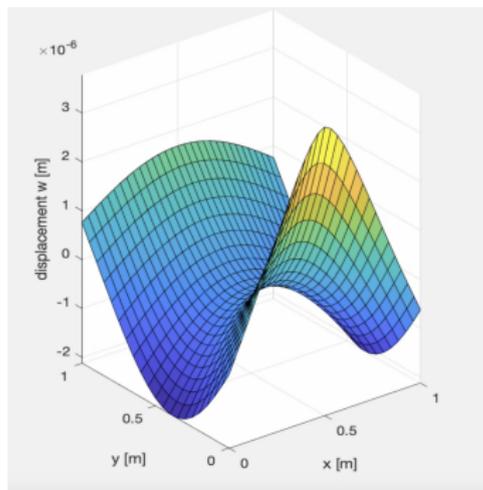
¹ Numerical simulation is performed by Daniel Veldman, a graduate PhD student from Eindhoven University of technology, The Netherlands.

Kirchhoff plate model-numerical solution

Inertia function ω_2 ¹



Compliance function ω_0 ¹



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Conclusion

Conclusion

- A general abstract formulation for the mechanical flexible system is studied at low frequency.
- The low order approximation is investigated for the boundary control systems.
- Numerical solution for the compliance function of the Kirchhoff plate is studied.

Publications and Secondments

Publications

- **"Time domain approach toward the calculation of the compliance function of flexible motion systems "** presented at 21st IFAC World Congress, Germany, July 11-17, 2020.
- **"Linear-time-varying feedforward control for position-dependent flexible structures"** presented virtually at European Control Conference (ECC 2020), 12-15 May, 2020.
- **"Compliance feedforward of flexible structures"** presented at the 38th Benelux Meeting on Systems and Control, Lommel, Belgium, 19 – 21 March, 2019.

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Secondments

Secondments	Supervisor's name	Date
Claude Bernard University	Prof.dr. B. Maschke	M16
ASML	Dr.ir. M. Heertjes	M23

My future next journey



Thank You !